

# The Utah urban carbon dioxide (UUCON) and Uintah Basin greenhouse gas networks: Instrumentation, data and measurement uncertainty

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10 **Abstract.** The Utah Urban CO<sub>2</sub> Network (UUCON) is a network of near-surface atmospheric carbon dioxide (CO<sub>2</sub>) measurement sites aimed at quantifying long-term changes in urban and rural locations throughout northern Utah since 2001. We document improvements to UUCON made in 2015 that increase measurement precision, standardize sampling protocols, and expand the number of measurement locations to represent a larger region in northern Utah. In a parallel effort, near-surface CO<sub>2</sub> and methane (CH<sub>4</sub>) measurement sites were assembled as part of the Uintah Basin Greenhouse Gas (GHG) network in a region of oil and natural gas extraction located in northeastern Utah. Additional efforts have resulted in automated quality control, calibration, and visualization of data through utilities hosted online (<https://air.utah.edu>). These improvements facilitate atmospheric modeling efforts and quantify atmospheric composition in urban and rural locations throughout northern Utah. Here we present an overview of the instrumentation design and methods within UUCON and the Uintah Basin GHG networks as well as describe and report measurement uncertainties using a broadly applicable and novel method. Historic and modern data described in this paper are archived with the National Oceanic and Atmospheric Administration's (NOAA) National Centers for Environmental Information (NCEI) and can be found at <https://doi.org/10.7289/V50R9MN2> and <https://doi.org/10.25921/8vaj-bk51> respectively.

## 1 Introduction

25 Increasing atmospheric carbon dioxide (CO<sub>2</sub>) caused by anthropogenic fossil fuel combustion is the primary driver of rising global temperatures (IEA, 2015), which has led to international commitment to reduce total carbon emissions. This includes the recent Paris Climate Agreement (Rohdes, 2016) which provided a framework for countries and sub-national entities to make carbon reduction commitments. Cities are playing an increasingly prominent role in these efforts including Salt Lake City, which has committed to a 50% reduction in carbon emissions by 2030 and an 80% reduction by 2040, relative to the baseline year of 2009 (Salt Lake City Corporation, 2016). Progress on emissions reduction efforts can be evaluated with accurate greenhouse gas measurements to provide trend detection and decision support for urban stakeholders and policymakers who are assessing progress on their mitigation efforts.

Data used to study modern near-surface atmospheric CO<sub>2</sub> mole fraction come from a variety of sources.

35 Flask-based sampling networks such as the one led by NOAA-Earth System Research Laboratory (Tans & Conway  
2005; Turnbull et al., 2012) offer long-term, globally representative records of several atmospheric tracers, however  
their measurement frequency is generally limited, and often do not capture intra-city signals. To supplement flask  
collection efforts, multiple tall tower greenhouse gas networks exist in North America (Zhao et al., 1997; Bakwin et  
al., 1998; Worthy et al., 2003; Andrews et al., 2014). These networks make continuous, calibrated CO<sub>2</sub>  
40 measurements and help to fill in the temporal gaps inherent to flask-based collection. However, by design tall towers  
are often located away from highly populated regions. Distance from urban emissions make tall tower measurements  
an invaluable tool for regional scale analysis and background estimates, but similar to flask collection networks they  
are unable to capture intra-city emissions signals.

While the majority of anthropogenic CO<sub>2</sub> emissions occur as a result of human activities in urban areas  
45 (Hutyra, 2014; EIA, 2015), most CO<sub>2</sub> monitoring sites are located away from urban sources to measure well-mixed  
mole fraction. Thus, long-term CO<sub>2</sub> mole fraction measured within urban areas are rare. Established in the year 2001  
(Pataki et al., 2003), the Utah Urban CO<sub>2</sub> Network (UUCON) is the longest running multi-site urban-centric CO<sub>2</sub>  
network in the world (Mitchell et al., 2018b) (Fig. 1 and 2).

UUCON collects near-surface data used to (a) understand spatial and temporal variability of emissions  
50 (Pataki 2003; Pataki et al., 2005; Mitchell et al., 2018b; Bares et al., 2018), (b) evaluate the accumulation of  
pollutants during complex meteorological conditions (Pataki et al., 2005; Gorski et al., 2015; Baasanbdorj et al.,  
2017; Bares et al., 2018, Fiorella et al., 2018), (c) develop and improve atmospheric transport models (Strong et al.,  
2011; Nehr Korn et al., 2013; Mallia et al., 2015), (d) validate emissions inventory estimates (McKain et al., 2012;  
Bares et al., 2018), (e) investigate relationships between urban emissions and air pollution, (Baasandorj et al., 2017;  
55 Mouteva et al., 2017; Bares et al., 2018), (f) and inform stakeholders and policymakers (Lin et al., 2018).

To leverage available infrastructure in urban environments and to increase the signals of intra-urban  
emissions, measurement sites within UUCON are located closer to ground level (Table 1) than tall tower  
measurement sites. Building-to-neighborhood-scale anthropogenic and biological fluxes contribute more strongly to  
the UUCON measurements relative to remote-location flask and tall tower observations. Studies comparing tower to  
60 near surface measurements in urban environments have identified an “urban canopy” effect that leads to elevated  
nocturnal mole fraction relative to higher above ground level (agl) measurements (Moriwaki et al., 2006). Thus, the  
near-surface UUCON data are applicable to research efforts, such as near field emission studies and smaller spatial  
scale analysis (~1 km<sup>2</sup> footprint, Kort et al., 2013) as well as mapping of spatial and temporal heterogeneities in  
urban emissions and intra-city modeling efforts (Fasoli et al., 2018).

65 In recent years, cities around the world have launched efforts to establish urban near surface CO<sub>2</sub>  
monitoring observatories for top-down emission estimates and for modeling validation efforts similar to the  
UUCON network (Mitchell et al., 2018b). These cities include Los Angeles (Duren and Miller, 2012; Newman et  
al., 2013; Verhulst et al., 2017), Indianapolis (Turnbull et al., 2015), Paris (Breon et al., 2015; Staufer et al., 2016),  
Rome (Gratani and Varone, 2005), Davos, Switzerland (Lauvaux et al., 2013), Portland (Rice and Nostrom, 2011),  
70 and Boston (Sargent et al., 2018), among others (Duren & Miller, 2012). In these studies the number of

measurement locations utilized is fewer than 5, many using a single measurement location to quantify city-wide CO<sub>2</sub> variability, with the notable exceptions of Indianapolis (Turnbull et al., 2015) and Los Angeles (Verhulst et al. 2017). While each of these studies employs somewhat similar measurement techniques, UUCON is unique in its length of record (Mitchell et al., 2018b).

75 Starting in 2015, the University of Utah deployed a network of high frequency, high precision instruments aimed at continuously measuring CO<sub>2</sub> and CH<sub>4</sub> from areas in eastern Utah where oil and natural gas extraction activities are prevalent (Figs. 2 and 3). This network is known as the Uintah Basin GHG network. These efforts were built on work previously conducted estimating fugitive CH<sub>4</sub> emissions (Karion et al., 2013) and the resulting local air quality problems (Edwards, 2013; Edwards et al., 2014; Koss et al., 2015). The methods developed for the  
80 measurements in the Uintah Basin GHG network have also been adopted at two UUCON sites to add CH<sub>4</sub> observations to the urban CO<sub>2</sub> record.

The aim of this paper is to describe the UUCON and Uintah Basin GHG measurement procedures, site locations and data structure with sufficient detail to provide documentation for analyses using these datasets, thereby serving as an in-depth methods reference. Furthermore, we developed a novel method for exploring and quantifying  
85 the measurement uncertainty which was used to analyse the performance of the network over multiple years, to provide insight into appropriate applications of the data, and to explore differences in data collection methods and instrumentation types. This unique method does not require the presence of a target tank within the dataset, allowing for it to be broadly applicable to many trace gas and air quality datasets that are limited to calibration information alone.

## 90 **2 Network Overview**

Currently, UUCON is comprised of nine sites that are dispersed across northern Utah (Fig. 1, Table 1). Six of the sites are in the Salt Lake Valley (SLV), the most heavily populated area of Utah with over 1 million residents as of this writing and where Salt Lake City, the state capital is located. The SLV is surrounded by mountains on all sides except for the northwestern part, where it borders the Great Salt Lake (Fig. 1). Sites in the SLV span multiple  
95 characteristics and land uses including residential, mid-altitude, mixed-use industrial, and rural. Two additional sites are located in the rapidly developing surrounding Heber and Cache Valleys, where the towns of Heber City and Logan are located. Both sites in the developing surrounding valleys are located in predominately residential or mixed commercial zones. In addition to the valley-based sites, a nearby high altitude CO<sub>2</sub> monitoring station (HDP), originally started and maintained by the National Center for Atmospheric Research as part of the Regional  
100 Atmospheric Continuous CO<sub>2</sub> Network in the Rocky Mountains (RACCOON; Stephens et al., 2011), has monitored CO<sub>2</sub> levels that serve as a regional background. The HDP site transitioned into the UUCON network in Fall 2016, at which time CH<sub>4</sub> observations were added, and continues to be maintained by the University of Utah.

Additionally, the University of Utah maintains a network of three greenhouse gas (GHG) monitoring sites in the Uintah Basin of eastern Utah, where energy extraction is taking place, measuring both CO<sub>2</sub> and CH<sub>4</sub> (Figs. 1,  
105 2, & 3; Table 1). The measurement techniques used in the Uintah Basin GHG network differ from UUCON in several ways including the use of a different analyzer and will be discussed in detail in Sections 2.2 and 4.1. These

methods have been adapted at two sites within the UUCON network (HDP and UOU) in an effort to add more GHG measurements (CH<sub>4</sub>) to the data record.

## 2.1 UUCON Instrumentation

110 Starting in 2001, researchers at the University of Utah deployed Li-6262 (Li-Cor inc., Lincoln, NE)  
infrared gas analyzers (IRGA) to measure CO<sub>2</sub> mole fractions in the SLV. Previous papers have described various  
different phases of the initial measurement sites (Pataki et al., 2003, 2005, 2006, 2007) (Fig. 2). This paper will  
focus on the methods and instrumentation developed in 2014 and implemented across the network by summer of  
2016, as well as the methods developed for the Uintah Basin GHG network (Fig. 3). Much of the equipment and  
115 materials used during the original phase of the network informed the selection of materials for the 2015 overhaul;  
however, all components with the exception of the IRGA's were replaced or rebuilt completely and the methods  
driving these components are significantly different or improved compared to the original design. Additional  
components were added to increase the functionality, stability and the maintenance of measurement sites (Fig. 4).

At each site, sample gas is continuously passed through the sample cell of a Li-6262 to measure CO<sub>2</sub> and  
120 H<sub>2</sub>O mole fractions (Fig. 4, Sect. 2.1.1). A small positive pressure is maintained throughout the analyzer and  
measurement system to make the identification of leaks easier and to reduce the impact on the accuracy of data in  
the event of a leak. Data is recorded as 10-second integrations of 1-second scans.

The historic method was a non-continuous method, which collected data on a 5 minute interval. Every 5  
minutes a pump would turn on and flow gas for 90 seconds then turn off and the system would then wait 30 seconds  
125 for the IRGA to reach a stable pressure. After the stabilization period data was recorded by a datalogger as a 1-  
minuet average of 10 second scans. The system would then sit idle, with out flowing gasses or recording data until  
the next sample period.

The decision to change from the historical method to one that continuously flows gas and collects data was  
in an effort to better capture higher frequency variations in observed values that could indicate near-field emissions.  
130 High frequency data allow for easier identification highly localized emissions (e.g., furnace, car) that can affect the  
signal at a site. Finally, while current atmospheric models are limited in their ability to address near field emissions  
effectively, advances in modeling efforts and computational resources makes this type of analysis feasible in the  
near future (Fasoli et al., 2018). Thus the high frequency collection of UUCON data is in anticipation of future  
model and analysis needs.

135 Multiple additional measurements are made to ensure the site's reliable performance, increase measurement  
accuracy, and to assist in identifying instrumentation problems when they arise (Sect. 2.1.7). All data are  
downloaded and displayed in real time on a public website (<http://air.utah.edu>) to reduce the time required to  
identify equipment failure and to provide public outreach. Pressure and water vapor broadening corrections, as well  
as data calibration, are performed post data collection and will be described in depth later (Sect. 3). Two sites in the  
140 UUCON network, UOU and HDP (Table 1), host an Ultra Portable Greenhouse Gas Analyzer (915-0011, Los Gatos  
Research, San Jose, CA) onsite. These sites use similar methods as those instrumented with the Li-6262 and will be  
discussed in-depth in section 2.2.



Lastly, the historic measurement design of UUCON included a 5-liter mixing buffer, which provided a physical mechanism for smoothing atmospheric observations and reducing instances of large deviations in observations. After moving to a continuous flow design, the buffer has been removed to enable us to measure high frequency variations. Smoothing can still be achieved at the post-processing and data analysis stages.

### **2.1.1 Infrared Gas Analyzer (IRGA)**

A Li-6262 infrared gas analyzer (IRGA) continuously measures CO<sub>2</sub> and H<sub>2</sub>O mole fraction. The IRGA contains two optical measurement cells and quantifies CO<sub>2</sub> mole fraction as the difference in absorption between the two cells with a 150um bandpass optical filter centered around 4.62 μm. To achieve a mole fraction measurement relative to zero, a CO<sub>2</sub> free gas (ultra-high purity nitrogen) is flowed through the reference cell while the gas of interest is passed through the sample cell (Fig. 4).

### **2.1.2 Datalogger**

A Campbell Scientific datalogger (CR1000, Campbell Scientific, Logan, UT) acts as both a measurement interface and control apparatus at each site. The datalogger records serial data streams from the gas analyzer, as well as analog voltage measurements from the gas analyzer and all additional periphery measurements. Periphery measurements include: flow rates, room temperature, sample gas pressure, sample gas temperature, and sample gas relative humidity. Several sites have additional air quality measurements that are recorded by the CR1000 (Table 1) which are not discussed here. The CR1000 is also responsible for driving the calibration periphery that introduces standard gases to the IRGA every two hours (Sect. 2.1.7).

### **2.1.3 Pump and Sample Loop Bypass**

Atmospheric sample air is pulled from the inlet to the analyzer using a 12-volt chemically resistant micro diaphragm gas pump (UNMP850KNDC-B, KNF Neuberger Inc., Trenton, NJ) that provides a reliable flow of 4.2 L/min. This flow rate is substantially higher than the 0.400 L/min sample flow rate selected for use at the analyzer. Thus, the pump is located upstream of the manifold where a sample loop bypass provides an alternative exit for unused sample gas. This loop is comprised of at least 9 meters of ¼" outer diameter (OD) (1/8" inner diameter) Bev-A-Line to provide sufficient resistance to the gas so when the manifold is open, gas passes through the mass flow controller and into the analyzer at the desired rate without losing all of the gas to the sample loop bypass (Fig. 4).

Since the pump is located upstream of the analyzer there is potential for CO<sub>2</sub> to absorb onto the material within the pump head and interfere with the atmospheric sample. The pumps used in the UUCON network were selected to minimize any potential interference with the sample. The diaphragms are made of a PTFE coated EPDM rubber which has been shown to have minimal gas phase absorption. Multiple laboratory and field tests were performed to verify that the location of the pump upstream of the analyzer would not impact the observations. No measureable impacts were identified provide us with a reasonable level of confidence that any absorption or interference from the pump is negligible.

### **2.1.4 Relays, Manifold and Valves**

Switching from sample gas to calibration gases is achieved using a six position 12-volt relay (A6REL-12, Campbell Scientific, Logan, UT), triggered by the datalogger at a known interval, connected to a six-port gas manifold (Ev/Et 6-valve, Clippard Instrument Laboratory, Inc., Cincinnati, OH) housing 12-volt Clippard relay valves (ET-2-12, Clippard Instrument Laboratory, Inc., Cincinnati, OH). Thus, when the program on the datalogger specifies, the CR1000 triggers a relay closing the sample valve and introducing a gas of known CO<sub>2</sub> mole fraction. Since the maximum number of gases used at each sampling location is five, the unoccupied position on the relay is often used to power the atmospheric sample pump.

### 2.1.5 Mass Flow Controller

A Smart-Trek 50 mass-flow controller (Sierra Instruments, Monterey, CA) is located between the manifold and analyzer to hold the sample flow consistent at 0.400 SL/minute (Fig. 4). Flow rates are recorded by analog measurement to the CR1000 to ensure a positive pressure remains consistent, and to help identify measurement issues remotely.

### 2.1.6 Calibration Materials

Each site houses three whole-air, high-pressure cylinders with known CO<sub>2</sub> mole fraction which are directly linked to World Meteorological Organization X2007 CO<sub>2</sub> mole fraction scale (Zhao and Tans, 2006), which generally last around one year in the field. Every two hours, the three calibration tanks are introduced to the analyzer in sequence. Each transition of gas begins with a 90 second flush period proceed by a 50 second measurement period, or two hours (minus calibration time) in the case of atmospheric sampling.

The molar fractions of calibration gases are chosen in an effort to span expected atmospheric observations. Values of the three reference materials are chosen to align with the 5<sup>th</sup>, 50<sup>th</sup>, and 95<sup>th</sup> percentile of the previous year's seasonal network wide observations (Fig. 5). Utilization of previous observations as a reference allows for a guided estimate of expected observations, thereby allowing for a minimization of interpolation without increasing extrapolation significantly, thus limiting extrapolation bias during calibrations.

In addition to the standard calibration gases, a long-term target tank is introduced to the analyzer every 25 hours. This tank is used to quantify performance of the site as well as determining the accuracy of post-processed calibrated data. The interval of 25 hours was selected to ensure that the calibration occurs at a different time each day in order to remove any consistent diel basis, and to prevent the loss of atmospheric observations at a reoccurring time. The target tanks were targeted to be slightly elevated above ambient mole fraction, with the average of 432.02 ppm CO<sub>2</sub>.

Calibration gases are produced in-house using a custom compressor design. 29.5 L volume N150 CGA-590 aluminum tanks are filled with city air using a high-pressure oil free industrial compressor (SA-3 and SA-6, RIX Industries, Benicia, CA). This system is similar to NOAA-ESRL Global Monitoring Division's (GMD) system (<http://www.esrl.noaa.gov/gmd/ccl/airstandard.html>). Water is removed prior to the tanks using a magnesium perchlorate trap to guarantee a dry gas. Tanks are spiked using a ~5,000 ppm dry CO<sub>2</sub> tank allowing for a wide range of targeted mole fractions depending on the season and expected range of observed atmospheric observations.

This spike tank was filled in the calibration lab by taking an aliquot from a 100% CO<sub>2</sub> gas cylinder and filling it with dried atmospheric air. To produce sub-ambient calibration tanks, tanks are mixed with a diluent made from atmospheric air scrubbed with a soda lime and magnesium perchlorate trap.

215 Our facility maintains a set of nine standard tanks originally calibrated by NOAA-ESRL's GMD that range from 328 to 800 ppm (during 2000-2004, directly linked to WMO Primary cylinders). Five of the original laboratory primary tanks were re-measured by GMD in 2011-2012 and were found to be lower than the originally measured CO<sub>2</sub> mole fraction by 0.10 to 0.51 ppm.

220 Laboratory primary tanks (which span 350 – 600 ppm) are propagated from the above into “laboratory secondary” tanks using a dedicated Li-7000 (LI-COR Biosciences, Lincoln, NE), and these are used in groups of 5 to calibrate working “tertiary” tanks used in the field. Secondary tanks are replaced as needed; since measurements began, nine secondary tanks have been used. Secondary calibration tanks are periodically re-measured relative to the WMO-calibrated tanks and are generally within 0.5 ppm of the original measurement. To assign a known mole fraction number to tertiary working calibration tanks, each tank is measured over a minimum of two days, with a  
225 minimum of three independent measurements per day. In a recent laboratory intercomparison experiment (WMO Round Robin 6), our facilities results were within 0.1 ppm of established WMO values ([https://www.esrl.noaa.gov/gmd/ccgg/wmorr/wmorr\\_results.php](https://www.esrl.noaa.gov/gmd/ccgg/wmorr/wmorr_results.php)).

The same methods used for developing laboratory primary, secondary and tertiary CO<sub>2</sub> tanks were used for CH<sub>4</sub> calibration materials with 5 original tanks spanning from 1.489 – 9.685 ppm CH<sub>4</sub>. Two of these tanks are  
230 directly tied to the WMO X2004A scale (Dlugokencky et al., 2005). These tanks are propagated into laboratory standards using a dedicated LGR-Greenhouse Gas Analyzer (Los Gatos Research, 907-0011, San Jose, CA). The spike tank used to produce elevated CH<sub>4</sub> calibration tanks was generated using the same method as the CO<sub>2</sub> spike tank, but using an aliquot from a 998 ppm CH<sub>4</sub> cylinder purchased from Airgas, Inc (Pennsylvania) and filling it with dried atmospheric air.

235 As shown in Figures 2 & 5, winter time CO<sub>2</sub> mole fraction in the SLV can reach over 650 ppm, with the 95<sup>th</sup> percentile over 550 ppm. As global CO<sub>2</sub> mole fraction increase in parallel with increasing populations in the SLV and urban areas of the Wasatch Front (Herbeke et al., 2014), the frequency and amplitude of these highly elevated observations will increase. Currently the WMO X2007 CO<sub>2</sub> scale has a maximum mole fraction of 521.419 ppm. Thus, the current WMO scale may be inadequate for urban observations in the SLV and the announced  
240 expansion of the WMO scale to 600 ppm will greatly benefit the urban trace gas community, which needs additional high-quality gas standards with mole fractions more appropriate to urban observations.

### 2.1.7 Additional Measurements

Three additional measurement sensors were added to the downstream side of the IRGA on the sample line to provide additional data for identifying equipment failure and to increase the accuracy of dry mole measurements. A  
245 pressure transducer (US331-000005-015PA, Measurement Specialties Inc., Hampton, VA) is located closest to the analyzer to represent pressures in the sample cell of the IRGA. This data stream is used for post processing pressure-broadening and water dilution corrections. Uncertainties in the precision and long-term stability of H<sub>2</sub>O mole

fraction measurements performed by the IRGA, due to a lack of frequent calibrations of water vapor, led to the addition of a relative humidity sensor (HM1500LF, Measurement Specialties Inc., Hampton, VA) and a direct immersion thermocouple (211M-T-U-A-2-B-1.5-N, Measurement Specialties Inc., Hampton, VA) for gas relative humidity and temperature measurements performed immediately after the pressure transducer respectively (Fig. 4). These measurements are utilized to calculate atmospheric H<sub>2</sub>O ppm, which is used to calculate CO<sub>2</sub> dry mole fraction and correct for water vapor broadening (Sect. 3.3).

### **2.1.8 Network Time Protocol**

Inter-site comparison and modeling applications require a high degree of confidence in the time stamp represented in data files. To verify the time stamps are consistent between sites and accurate, a network time check is executed every 24 hours at 00:00 UTC. If the difference between the network clock and the clock on the datalogger is greater than 1000 microseconds, the datalogger clock is reset to match the network clock. All times are recorded in UTC to avoid potential confusion associated with daylight savings. Network time checks and data transfers are established via internet connections at each site either through existing Ethernet connections or cellular modems (RV50, Sierra Wireless, Carlsbad, CA).

## **2.2 Uintah Basin GHG Network Instrumentation**

The Uintah Basin GHG network utilizes the Los Gatos Research Ultra-Portable Greenhouse Gas Analyzer (907-0011, Los Gatos Research Inc., San Jose, CA), hereafter referred to as “LGR” at all three sites within the network (Fig. 6). Unlike the UUCON network, in which the measurement system and its peripherals are essentially a custom engineered solution of an array of different components from multiple manufacturers brought together by the researchers running the network, the LGR sites employ systems fully designed by a single manufacturer. The use of an “off the shelf” unit like that deployed in the Uintah Basin GHG network has both advantages and disadvantages. The barrier of entry is much lower and does not require advanced programming abilities. However, the increase in ease of use results in a decrease in the flexibility of operation, and in some cases the measurement precision decreases (Sect. 4.1).

The Uintah Basin GHG network has supported several recent projects including Foster et al., 2017 and Foster et al., 2019, in which the data collected from this network were used to estimate and confirm basin wide CH<sub>4</sub> emissions and examine CH<sub>4</sub> emissions during wintertime stagnation episodes respectively. In an effort to minimize differences between the two networks, measurement frequency, networking, calibration materials (Sect. 2.1.6), and post processing calibration methods (Sect. 3.1) all follow the same protocols described for the UUCON network with the notable exception of the calibration frequency, which is every three hours as opposed to every two with the Li-6262's.

### **2.2.1 LGR Calibrations**

Calibration gases are introduced to the analyzer every three hours using three whole-air, high-pressure reference gas cylinders with known CO<sub>2</sub> and CH<sub>4</sub> mole fraction that are directly linked to the WMO X2007 CO<sub>2</sub> mole fraction scale (Zhao and Tans, 2006) and the WMO X2004A CH<sub>4</sub> mole fraction scale (Dlugokencky et al., 2005) as

described in section 2.1.6. Molar fraction of CH<sub>4</sub> calibration gasses are chosen to align with the 5<sup>th</sup>, 50<sup>th</sup> and 95<sup>th</sup> percentile of the previous years observations, while CO<sub>2</sub> gasses match those described in section 2.1.6. Calibration gases are introduced using an LGR Multiport Input Unit (MIU-9, Los Gatos Research Inc., San Jose, CA). H<sub>2</sub>O mole fractions are calibrated using a Li-Cor Li-610 dew point generator (Li-Cor inc., Lincoln, NE) approximately every three months.

### 2.2.2 LGR H<sub>2</sub>O and Pressure Corrections

The LGR analyzer measures mole fraction of H<sub>2</sub>O, CO<sub>2</sub> and CH<sub>4</sub>, the later two of which are impacted by the presence of water vapor in the sample and the pressure within the cavity of the instrument. Corrections for pressure, water vapor dilution and spectrum broadening for CH<sub>4</sub> and CO<sub>2</sub> are made on-site by LGR's software and validated empirically by laboratory testing using calibration gasses of know concentrations and the same Li-610 dew point generator described above, which generates a stable dew point at a set temperature (+/-0.2 °C). Independent error estimates of the LGRs H<sub>2</sub>O correction were produced (Sect. 4, Table 3) resulting in an average uncertainty of 0.017 ppm CO<sub>2</sub>.

### 2.2.3 LGR Additional Considerations

The addition of a target tank, as described in section 2.1.6, would be greatly beneficial for analyzing the long-term performance of each measurement site. However, the current version of the LGR proprietary software that drives the MIU calibration unit lacks flexibility to accommodate a calibration sequence independent of a standard sequence and thus a target tank was not implemented in the Uintah Basin GHG network design.

## 3 Data and Post Processing

For both the UUCON and the Uintah Basin GGA network, raw data are pulled from each site on a 5-minute interval to the Center for Higher Performance Computing at the University of Utah. Data are then run through an automated calibration and quality assurance program described below and made publicly available at <https://air.utah.edu>.

### 3.1 Calibrations

Data from UUCON measurement sites with a Li-6262 on site (Table 1) are calibrated every two hours using the three reference gases outlined in section 2.1.6, while sites with a LGR are calibrated every three hours. Since the Li-6262's are near linear through the range of atmospheric observations and calibration gases, each standard of known mole fraction is linearly interpolated between two consecutive calibration periods to represent the drift in the measured standards over time (Fig. 7). Ordinary least squares regression is then applied to the interpolated reference values and the linear coefficients are used to correct the observations (Fig. 7). The linear slope, intercept, and fit statistics are returned for each observation for diagnostic purposes.

### 3.2 Pressure Corrections

Changes in ambient atmospheric pressure can impact the measurement of CO<sub>2</sub> mole fraction. Pressure effects can be mathematically accounted for, or minimized or eliminated by maintaining a constant flow in the optical cavity during calibration and atmospheric sampling periods, as well as calibrating at a high enough frequency that differences in atmospheric pressure between calibration periods is minimal. To account for pressure, the LGR's control the pressure with in the cavity and maintaining a near constant 140 torr. The Li-6262's in the UUCON network do not have mechanisms for controlling the pressure within the cavity and thus implement the latter strategy described above, calibrating frequently and standardizing the flow of gasses through the optical cavity.

### 3.3 Water Vapor Calculations and Corrections

To report dry mole fractions, the presence of water vapor (H<sub>2</sub>O) must be accounted for. The presence of water vapor impacts measured CO<sub>2</sub> mole fraction through both pressure dilution and spectral band broadening. Both of these effects are corrected for during the post processing of UUCON data while the LGR sites rely on LGR's internal software. H<sub>2</sub>O mole fraction are calculated using the relative humidity, pressure and temperature measurements (Sect. 2.1.7) to first determine saturation vapor pressure utilizing the Clausius-Clapeyron relation with Wexler's equation (Wexler, 1976) below:

$$\ln e_s = \sum_{i=0}^6 g_i T^{i-2} + g_7 \ln(T) \quad (1)$$

where  $e_s$  is the saturation vapor pressure in Pa,  $T$  is the temperature in Kelvin and coefficients  $g_0 - g_7$  are as follows respectively:  $-0.29912729 \times 10^4$ ,  $-0.60170128 \times 10^4$ ,  $0.1887643854 \times 10^2$ ,  $-0.28354721 \times 10^{-1}$ ,  $0.17838301 \times 10^{-4}$ ,  $-0.84150417 \times 10^{-9}$ ,  $0.44412543 \times 10^{-12}$ ,  $0.2858487 \times 10^1$ .

Vapor pressure ( $e$ ) is calculated using  $e_s$  from equation 1:

$$e = e_s \times \frac{RH}{100} \quad (2)$$

H<sub>2</sub>O mole fraction is then calculated by taking the ratio of vapor pressure ( $e$ ) over total atmospheric pressure ( $P$ ) and converting to parts per million (ppm).

$$H_2O = \frac{e}{P} \times 1000000 \quad (3)$$

Due to the law of partial pressures, the presence of H<sub>2</sub>O decreases measured CO<sub>2</sub> mole fraction. As the amount of H<sub>2</sub>O increases, the CO<sub>2</sub> mole fraction must decrease for atmospheric pressure to remain unchanged. Using calculated H<sub>2</sub>O from equation 1, 2 and 3 we correct for the dilution effect of H<sub>2</sub>O on the measured atmospheric CO<sub>2</sub> using the following equation:

$$CO_{2d} = CO_{2w} \left( \frac{1}{1 - H_2O} \right) \quad (4)$$

where  $CO_{2w}$  is the “wet sample” of atmospheric  $CO_2$  and  $CO_{2d}$  is the dry air equivalent. Given realistic atmospheric values for the summer in the SLV, 10,000 ppm  $H_2O$  and 400 ppm  $CO_2$ , the dilution correction described in equation 4 will result in a positive 4.04 ppm  $CO_2$  offset ( $CO_{2d} = 404.04$  ppm).

345 The infrared absorption band utilized by the Li-6262’s deployed in the UUCON network is broadened by presence of  $H_2O$  resulting in a decrease in the measured  $CO_2$  mole fraction. To correct for this effect on the measured  $CO_{2w}$  described in equation 4, we calculated the  $CO_{2d}$  in equation 5:

$$\begin{aligned}
 Y_c(CO_{2w}) &= \frac{a + b \times CO_{2w}^{1.5}}{a + CO_{2w}^{1.5}} + c \times CO_{2w} \\
 CO_{2d} &= CO_{2w}(1 + 0.5H_2O)(1 - 0.5H_2O \times Y_c(CO_{2w}))
 \end{aligned}
 \tag{5}$$

350 where  $a = 6606.6$ ,  $b = 1.4306$ , and  $c = 2.2462 \times 10^{-4}$  and details regarding function  $Y_c$  can be found in Li-cor technical documentation (App Note #123).

Using the same values of 10,000 ppm  $H_2O$  and 400 ppm  $CO_2$ , the above equation will result in a -0.66ppm change. Thus the net correction for both pressure broadening (Eq. 4) and dilution effect (Eq. 5) using the same theoretical  $H_2O$  and  $CO_2$  mole fraction results in a 403.3 ppm  $CO_2$  dry mole fraction with in the UUCON network.

### 3.4 Data Files

355 Data are stored at three different levels: raw, QA/QC, and calibrated. Data are stored in monthly files at the native 10-second frequency for all three levels. Raw and QA/QC data files contain an identifier of which gas is currently being measured with atmospheric air identified as -10, flush periods as -99, and standard mole fraction identified as their known mole fraction (i.e. 405.06 ppm).

360 The lowest level raw data are stored in the same format when pulled from the datalogger at the measurement sites. No periods of data are removed from this level and no corrections or calibrations are applied, thus remaining totally unaltered.

The second level of data, QAQC, remains in a similar structure as raw data with a few key exceptions. First, user specified bad data is removed. A text file containing the periods of “bad data” is maintained for each site, which is read by automated scripts to remove selected periods. This is a fairly flexible format for removing periods of suspect data that can be easily updated allowing for quick reprocessing of data. Second, automated quality control scripts are run and a column of quality assurance flags are added (Table 2). Lastly, calculation of  $H_2O$  mole fraction is performed and  $CO_2$  dry mole fraction is calculated as described in section 3.3.

370 The third and highest level of data, calibrated data, are generated using the QAQC data files. Periods of invalidated records that fail the automated quality control scripts are removed, and calibrations are applied to all remaining data.

### 3.5 Sample Sequence

Since all UUCON measurement sites have only one inlet height, atmospheric sampling is continuous between calibration periods, with no data loss associated with transition periods between sample inlets. During atmospheric

sampling, air is drawn from the inlet and passed through the analyzer continuously where it is identified (ID) as the numerical value -10 in the raw and QA/QC data files. Every two hours, all three of the calibration materials on site are introduced to the analyzer in sequence, with a 90 second flush period (ID = -99) to allow for equilibration and full change-over of the sample cell, followed by 50 seconds of measurement time, resulting in a total of 140 seconds per calibration gas. Figure 7 shows the transition from atmospheric air to a standard gas and the time required to reach equilibration. Every 25 hours, a target tank is introduced half way through the hour (i.e., 07:30) using the same sequence described above, but treated as an unknown and not utilized in the calibration routine described in section 3.1.

#### 4 Calculating Measurement Uncertainties

A critical feature of any atmospheric measurement system is an assessment of the system's associated measurement uncertainty. A comprehensive analysis of greenhouse gas measurement uncertainties has been described for the NOAA tall tower network (Andrews et al., 2014) and for the LA Megacities project (Verhulst et al., 2017). Here we have not estimated exhaustively every possible error source. Instead, we have focused on creating a running uncertainty estimate through time that is similar to the approach taken in the INFLUX project (Richardson et al., 2017). Due to the importance of water vapor on the accurate measurement of a CO<sub>2</sub>, especially in a measurement system that does not dry the atmospheric sample like the two describe in this paper, we have produced and reported uncertainty estimates for H<sub>2</sub>O vapor measurements ( $1\sigma U_{h_2o}$ ) as it impacts CO<sub>2</sub> as well as observed analyzer precision ( $1\sigma Up$ ) in the field (Table 3). We do not report a total, accumulative uncertainty estimate from all possible sources of error combined. Uncertainties beyond those reported here are small compared to the running uncertainty estimate and could be estimated in future work.

One method for estimating measurement uncertainties is to use a validation reference gas tank, or "target tank" ( $U_{TGT}$ ). The target tank is similar to the other calibration gas tanks, but it is not used to calibrate the data and is also sampled at a lower temporal frequency (once every 25 hours; Sect. 2.1.7). Since the UUCON network design encompasses a target tank we are able to leverage this method to estimate uncertainty within the network. An example of the target tank measurement is shown in the right panel of Figure 7, where the target tank was measured at 07:30 UTC. The target tank measurements are treated as an unknown and calibrated (Sect. 3.1). The absolute value of the difference between the post-calibrated and known values of the target tank is then calculated. We smoothed the absolute difference time series by convolving it with an 11-point Gaussian window derived according to:

$$e^{-\frac{1}{2}\left(\alpha\frac{n}{(N-1)/2}\right)^2} \quad (6)$$

where  $\alpha$  is 2.5,  $N$  is the number of points (11), and  $n$  is the sequence between  $(N-1)/2 \leq n \leq (N-1)/2$ . Prior studies have also used smoothed target tank values to represent measurement uncertainty through time; however, each research group has used a different method. For instance, in the NOAA tall tower network, the  $1\sigma$  absolute value of the difference between the measured and known target tank mole fractions was calculated across a 3-day processing window (Andrews et al., 2014). In the LA Megacities project, the root mean square error (RMSE) across



11 target tank measurements (measured every 22 hours) was used (Verhulst et al., 2017). Finally, in the INFLUX  
410 project a running standard deviation of the absolute value of the difference between the measured and known target  
tank mole fractions over 30-days was used (Richardson et al., 2017). While these approaches differ in their details,  
each represents an assessment of  $U_{TGT}$  through time. Future work could examine how the different target tank-based  
uncertainty estimates compare to each other and how they affect atmospheric inversion estimates.

Within the UUCON network, target tanks were incorporated into the experimental design in July 2017 at  
415 all of the sites with a Li-6262 analyzer, while sites equipped with a LGR analyzer did not host a target tank, as of  
this writing. Thus, to estimate the measurement uncertainty at the LGR sites as well as at Li-6262 sites prior to the  
deployment of the target tanks, an alternative measurement uncertainty method was needed. We produced a method  
that takes the calibration gas measurements at time  $t$ , treats them as pseudo target tanks, and interpolates the  
calibration gas measurements between the prior ( $t-1$ ) and next ( $t+1$ ) calibration periods to derive a slope and  
420 intercept at time  $t$  that is then used to calculate the calibrated mole fraction mixing ratios of the pseudo target tanks  
and derive an uncertainty estimate. An example of this process is shown in Figure 8 for the calibration on Nov 27,  
2017 at 18:00 UTC at the IMC site. The calibration gas measurements were interpolated between 16:00 ( $t-1$ ) and  
20:00 ( $t+1$ ) and used to obtain an interpolated slope and intercept at 18:00 ( $t$ ) (blue dashed line and triangles in Fig.  
8a). The interpolated slope and intercept can be compared to the actual values obtained from the usual calibration  
425 procedure (orange circles). The blue dashed line illustrating the interpolation procedure is only shown between  
16:00 and 20:00 for clarity, but this process was repeated for each calibration time period. The interpolated slope  
and intercept were then used to calibrate the pseudo target tank measurements at  $t$  (blue triangles in Fig. 8b). The  
RMSE between the calibrated and known values of the three pseudo target tanks was then calculated (grey circles in  
Fig. 8d). Since the RMSE can vary substantially between calibration points, we smoothed it by convolving it with an  
430 11-point Gaussian window to yield the pseudo target tank uncertainty, or  $U_{pTGT}$  (blue squares in Fig. 8d). For this  
example at 18:00, the interpolated calibration intercept resulted in a relatively large deviation of the calibrated  
pseudo target tank mole fractions from their known values that then resulted in an elevated RMSE. The elevated  
RMSE from this calibration point then persists for several calibration periods (hours) in the smoothed  $U_{pTGT}$ .

Once  $U_{pTGT}$  was calculated, we compared it to the traditional  $U_{TGT}$  over time at the IMC site (Fig. 9). For  
435 reference, the yellow shaded region in Figure 9 is the time period shown in Figure 8. In July-August 2017 at IMC  
there was a bias in the post-calibration target tank mole fractions that similarly affected the pseudo target tank  
RMSE values (Fig. 9d). In September 2017 the low concentration calibration tank was removed from the site for a  
month and the RMSE values of both metrics improved. Finally, in October 2017 a third calibration tank was re-  
installed and there was again a bias in the target tank and pseudo target tanks. The close fidelity through time  
440 between the  $U_{pTGT}$  and  $U_{TGT}$  metrics provides confidence that  $U_{pTGT}$  serves as a robust estimate of measurement  
uncertainty that is similar to what can be obtained with a traditional target tank. Finally, Figure 10 shows the entire  
 $CO_2$   $U_{pTGT}$  and  $U_{TGT}$  record at all of the sites, while Figure 11 shows the entire  $CH_4$   $U_{pTGT}$  record, with average  
values reported in Table 3. The  $U_{pTGT}$  is reported in the hourly averaged data files as our estimate of measurement  
uncertainty. It should be noted that since  $U_{pTGT}$  is time dependent, gaps in data will result in large uncertainties  
445 estimates. As a result we have added a mask, in which any period of data with 8 hours or more of missing data are

removed from the  $U_{pTGT}$  calculation. Additionally, bias in the assigned values of calibration tanks, as well as changes in the distribution of the mole fraction of calibration tanks on site, can result in result in step wise changes in  $U_{pTGT}$  as can be seen if figures 10 and 11.

450 The average absolute difference between  $U_{pTGT}$  and  $U_{TGT}$  at all measurement locations within the UUCON network was 0.03 ppm CO<sub>2</sub>, suggesting this metric is representative of a more directly measured uncertainty metric like  $U_{TGT}$  (Table 3).

455 Water vapor precision was examined using laboratory tests for the UUCON and the Uintah Basin GHG network designs and are reported in Table 3 ( $U_{h2o}$ ). Gas from a dry calibration tank of know CO<sub>2</sub> mole fraction was passed through a Li-610 dew point generator at a set dewpoint temperature. H<sub>2</sub>O measurements were collected by both systems in parallel over a period of 1.5 hours. We calculated the Allan variance to represent the precision of the H<sub>2</sub>O measurements regardless of drift over time or other systematic errors. This precision statistic was used to construct a normal distribution of H<sub>2</sub>O centered on the mean measured H<sub>2</sub>O mole fraction at each site, which is used to estimate the uncertainties in dry air equivalent estimates for CO<sub>2</sub> due to H<sub>2</sub>O repeatability error using methods discussed in section 3.3. The 1 $\sigma$  uncertainty of the H<sub>2</sub>O precision results in a mean 0.019 ppm CO<sub>2</sub> error ( $U_{h2o}$ ) for 460 the UUCON network, and 0.017 ppm CO<sub>2</sub> for the Uintah Basin GHG network design. These uncertainties represent a lower bounds for error in CO<sub>2</sub> resulting in H<sub>2</sub>O measurements as they do not account for errors in H<sub>2</sub>O measurement accuracy, which can be addressed during the QAQC of data.

#### 4.1 Instrument Differences and Uncertainties

465 A unique aspect of the UUCON and Uintah Basin networks is the use of two different instruments to measure CO<sub>2</sub>. This allows the ability to directly compare instrument performance during extended field operations. Table 3 shows the uncertainty metrics described in section 4 and in Figures 8, 9, 10 and 11. Additionally, the precision of the instruments ( $U_p$ ) at each site is reported as an average value of the standard deviation (1 $\sigma$ ) of the calibrated values for each individual calibration gas introduced to the analyzer since the overhaul of the site, the standard deviation (1 $\sigma$ ) of H<sub>2</sub>O measurements expressed in terms of uncertainty added to CO<sub>2</sub> ppm as determined by 470 lab tests, as well as the data recovery rates for each site. Site to site variability in  $U_{pTGT}$  ranges from 0.18 to 0.69 ppm CO<sub>2</sub> within the UUCON network, with the highest observed uncertainty at sites with more limited environmental controls and a mean value of 0.38 ppm across the entire network. Sites equipped with a LGR ranged from 0.17 to 0.36 CO<sub>2</sub> ppm (1.8 to 4.2 ppb CH<sub>4</sub>), with a mean across all sites of 0.25 ppm CO<sub>2</sub> (2.8 ppb CH<sub>4</sub>). Uncertainty in CO<sub>2</sub> ppm resulting from the measurement of H<sub>2</sub>O ( $U_{h2o}$ ) is minimal between sites (0.017 to 0.020 ppm CO<sub>2</sub>) and has a 475 minimal impact on CO<sub>2</sub> uncertainties. (Table 3)

Our reported average CH<sub>4</sub>  $U_{pTGT}$  uncertainty value of 2.8 ppb is notably higher than those reported by other groups quantifying measurement uncertainty, including Verhulst et al., 2017 which reported a value of 0.2126 ppb uncertainty as estimated using the post-calibrated target tank residuals integrated over 10 days of observations, and a total CH<sub>4</sub> uncertainty ( $U_{air}$ ) of 0.7224 ppb from measurements using a Picarro G2301 (Picarro Inc., Santa Clara, 480 CA). Our higher reported values are likely the result of both the use of a different analyzer than a Picarro, as well as

the fact that our uncertainty estimates are based on an interpolation between non-sequential calibration periods and not a directly measured target tank.

485 It is notable that in all but one instance that the precision ( $U_p$ ) of the Li-6262s CO<sub>2</sub> is twice as precise than the LGRs (Table 3), and the one instance is at DBK which experiences larger temperature ranges, despite the Li-6262s being ~20 years older than the LGRs. Additionally, the uncertainty and data recovery rates between the two instrument types are highly comparable.

The highly similar CO<sub>2</sub> metrics observed between the two instrumentation types suggests that the most significant advantage of the more modern direct absorption LGR's is the addition of a second gas species measured, methane (CH<sub>4</sub>) in this instance, especially at sites with well-regulated climate controls.

## 490 **5 Data Availability**

All data described in this paper are archived with the National Oceanic and Atmospheric Administration's (NOAA) National Centers for Environmental Information (NCEI) and can be found at <https://doi.org/10.7289/V50R9MN2> and <https://doi.org/10.25921/8vaj-bk51>.

## **6 Conclusions**

495 As the global effort to reduce greenhouse gas emissions transitions from commitment to policy measures, greenhouse gas measurement networks provide a means for evaluating progress. The UUCON network is an example of an urban CO<sub>2</sub> network well suited for this application due to its long-term duration, precision, and spatial distribution (Mitchell et al., 2018b). With high data recovery rates and low average measurement uncertainty ( $U_{pTGT}$ ) of 0.38 ppm CO<sub>2</sub>, the network produces data suitable for a range of scientific and, potentially, policy applications.  
500 Additionally, there is increasing interest in performing cross-urban comparisons between different urban environments. Given the reported measurement uncertainties, the frequency of calibrations and the tractability to international working scales, these data are well situated for this application.

The overhaul of instrumentation and design documented in this paper has resulted in a robust network of reliable data, with additional measurements to remotely identify when problems arise as well as increase the  
505 precision of the data. The standardization of materials and measurement protocols at all locations has significantly lowered the barrier of entry for maintenance of the sites.

The addition of target tanks at multiple sites in 2017 allows for the calculation of continuous uncertainty metrics. From those metrics, an interpolation method was developed allowing for uncertainty estimates of sites and networks where a target tank is not available. This novel method for estimating uncertainty provides useful insight  
510 into the quality of data produced at individual sites and is broadly applicable to any atmospheric trace gas or air quality dataset that contains calibration information.

The use of the interpolated uncertainty metric, as well as the calculation of the standard deviation of calibration measurements in the field, identified limited differences between the two measurement techniques used in the UUCON and Uintah Basin GHG networks.

515 Targeted reductions in the emissions of other greenhouse gases, primarily CH<sub>4</sub>, will require similarly  
distributed measurement networks for validating reduction progress and tracking emissions, both in urban areas and  
regions of oil and natural gas extraction. With three years of continuous operation to date, and relatively low  
measurement uncertainty (2.8 ppb CH<sub>4</sub>) the Uintah Basin GHG network serves as a good example of a greenhouse  
gas network with simultaneous measurements of CH<sub>4</sub> and CO<sub>2</sub>. With comparable precision and reliability as those  
520 reported in UUCON, but with the added benefit of two measurement species, the measurement techniques deployed  
in the Uintah Basin GHG network have been expanded into a few urban locations within the UUCON network.

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735 **Table 1:** Site Characteristics. Historic sites that have been relocated are not listed.

Site Code	Site Name	Latitude (N)	Longitude (W)	Elevation (m)	Inlet Height (m agl)	Species	Start Date; Overhaul Date*	Instrument	Land-Use
UOU	University of Utah	40.7663	111.8478	1,436	36.2	CO <sub>2</sub> , CH <sub>4</sub> , CO, O <sub>3</sub> , PM <sub>2.5</sub> , NO <sub>x</sub>	2001/02/07; 2013/10/09	LGR UP-GGA	Mixed residential commercial
SUG	Sugarhouse	40.7398	111.8580	1,328	3.86	CO <sub>2</sub> , PM <sub>2.5</sub>	2005/01/11; 2015/10/31	Li-6262	Residential
IMC	Intermountain Medical Center	40.6602	111.8911	1,316	66.0	CO <sub>2</sub>	2016/09/25	Li-6262	Commercial
RPK	Rose Park	40.7944	111.9319	1,289	3.25	CO <sub>2</sub>	2009/02/24; 2015/11/19	Li-6262	Residential
DBK	Daybreak	40.5383	112.0697	1,582	5.05	CO <sub>2</sub> , PM <sub>2.5</sub>	2004/01/21; 2015/09/29	Li-6262	Rural sagebrush steppe
HDP	Hidden Peak	40.5601	111.6454	3,351	17.1	CO <sub>2</sub> , CH <sub>4</sub>	2006/04/21; 2016/07/20	LGR UP-GGA	High Elevation / Urban Background
LGN	Logan	41.7616	111.8226	1,392	3.23	CO <sub>2</sub>	2015/07/27	Li-6262	Mixed Residential Commercial
HEB	Heber	40.5067	111.4036	1,721	4.20	CO <sub>2</sub>	2015/07/28	Li-6262	Residential Developing
SUN	Suncrest	40.4808	111.8371	1,860	4.22	CO <sub>2</sub>	2015/08/11	Li-6262	Mid-altitude, Residential
FRU	Fruitland	40.2087	110.8404	2,024	4.04	CO <sub>2</sub> , CH <sub>4</sub>	2015/03/19	LGR UP-GGA	Basin Background
ROO	Roosevelt	40.2941	110.0090	1,585	4.06	CO <sub>2</sub> , CH <sub>4</sub>	2015/03/23	LGR UP-GGA	Basin Residential
HPL	Horsepool	40.1434	109.4680	1,567	4.06	CO <sub>2</sub> , CH <sub>4</sub>	2015/01/28	LGR UP-GGA	Oil and Natural Gas

\* If there is only one date listed then the site is a new installation.

**Table 2: Quality Assurance and Control Flags**

<b>Flag</b>	<b>Descriptor</b>
-1	Data manually removed
-2	System flush
-3	Invalid valve identifier
-4	Flow rate or cavity pressure out of range
-5	Drift between adjacent reference tank measurements out of range
-6	Time elapsed between reference tank measurements out of range
-7	Reference tank measurements out of range
1	Measurement data filled from backup data recording source

**Table 3: CO<sub>2</sub> and CH<sub>4</sub> Measurement Uncertainties with Gaussian window target tank method ( $U_{pTGT}$ ), target tank ( $U_{TGT}$ ), analyzer precision at 1 $\sigma$  ( $U_p$ ), H<sub>2</sub>O measurement precision 1 $\sigma$  ( $U_{h2o}$ ) as expressed in ppm CO<sub>2</sub> uncertainty, and data recovery rates from UUCON and Uintah Basin GHG measurement averaged over the entire record since sites were overhauled.**

Site Code	CO <sub>2</sub> $U_{pTGT}$ (ppm)	CO <sub>2</sub> $U_{TGT}$ (ppm)	CO <sub>2</sub> 1 $\sigma$ $U_p$ (ppm)	CH <sub>4</sub> $U_{pTGT}$ (ppb)	H <sub>2</sub> O 1 $\sigma$ $U_{h2o}$ (ppm)	Data Recovery Rate
DBK	0.69	0.67	0.04	NA	0.019	0.82
HEB	0.22	0.37	0.04	NA	0.020	0.81
IMC	0.36	0.38	0.03	NA	0.020	0.71
LGN	0.18	0.50	0.04	NA	0.019	0.85
RPK	0.45	0.24	0.10	NA	0.019	0.83
SUG	0.30	0.19	0.04	NA	0.020	0.80
SUN	0.43	0.48	0.05	NA	0.019	0.73
UOU	0.36	NA	0.08	3.3	0.017	0.91
FRU	0.32	NA	0.13	2.7	0.017	0.86
HDP	0.17	NA	0.10	2.0	0.017	0.77
HPL	0.24	NA	0.08	4.2	0.017	0.77
ROO	0.18	NA	0.10	1.8	0.017	0.81

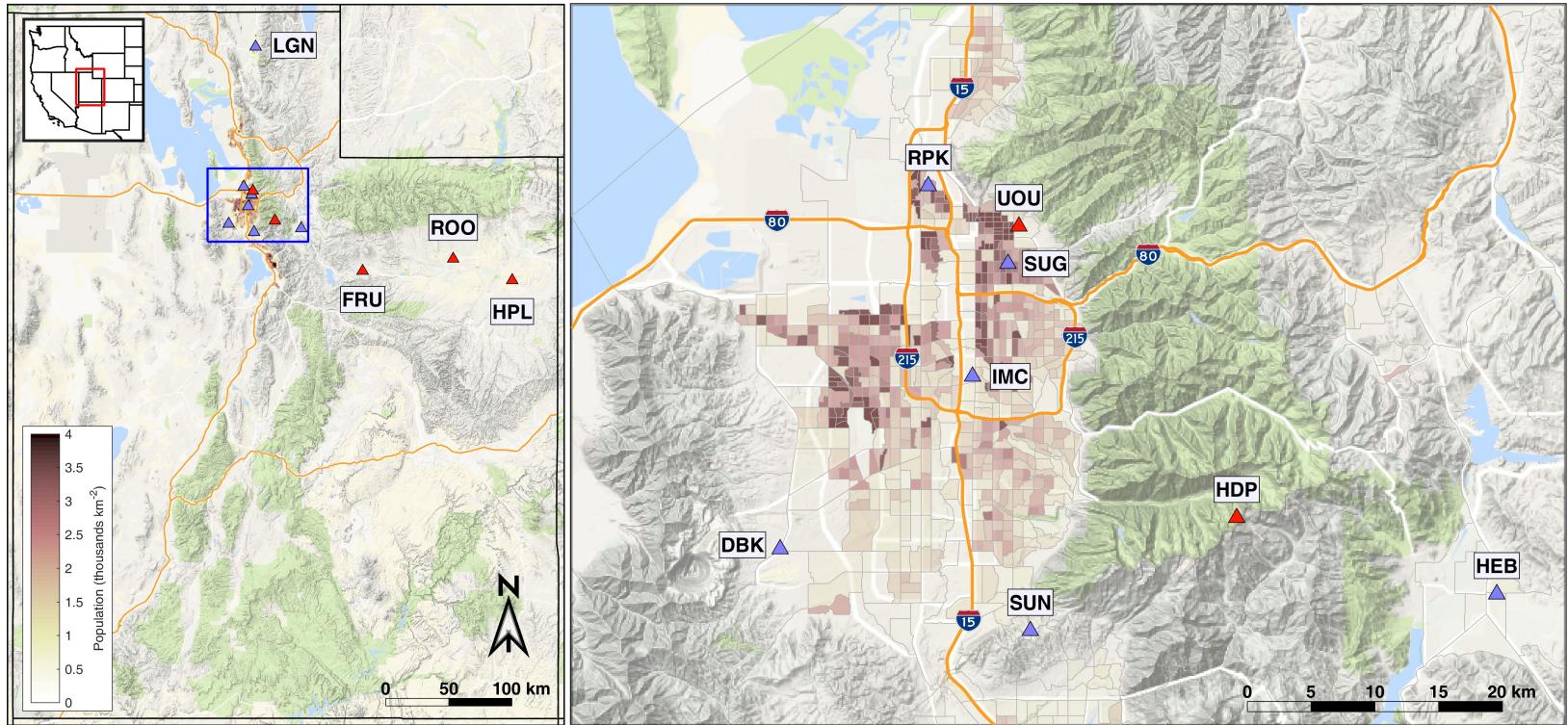


Figure 1: Map showing the location of UUCON and Uinta Basin GHG measurement sites. Left panel shows full distribution of sites in Utah with blue square indicates extent for the right panel. Right panel shows the Wasatch Front and the Salt Lake Valley in detail with population density in thousands per km<sup>2</sup>. Sites equipped with a Li-6262 identified with blue triangle and sites with an LGR UP-GGA identified with red triangle.

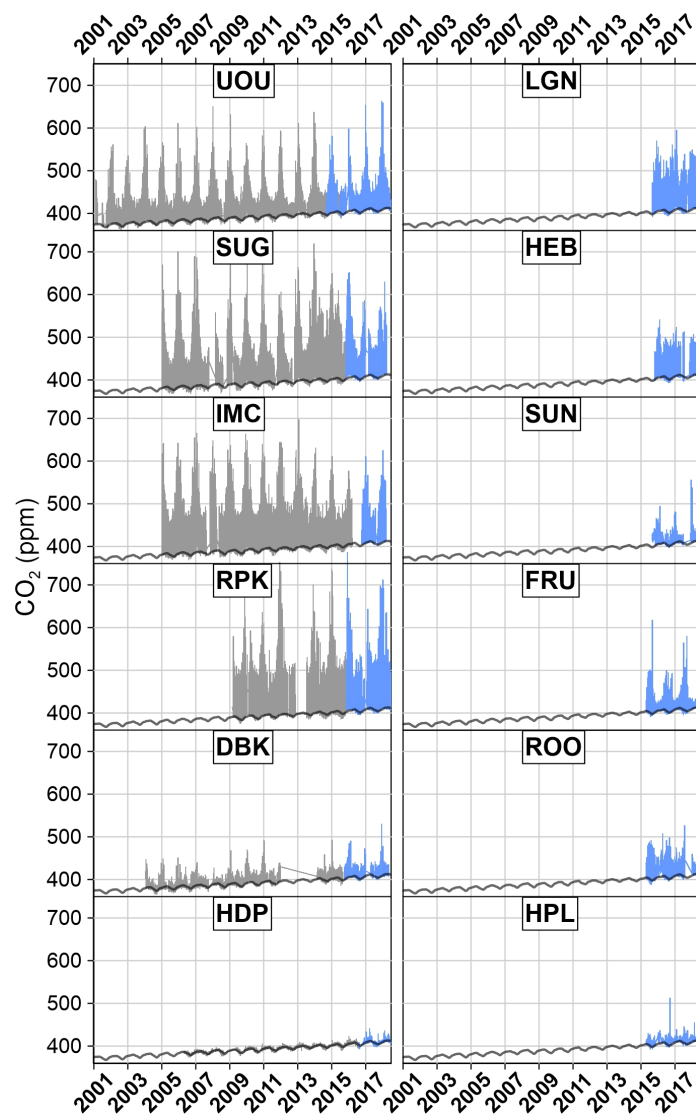


Figure 2: Full record time series of CO<sub>2</sub> measurements from the UUCON and Uintah Basin GHG. Measurement techniques and uncertainty covered in this manuscript indicated by blue with historic data represented in grey. Black line represents regional background as described in Mitchell et al., 2018a.

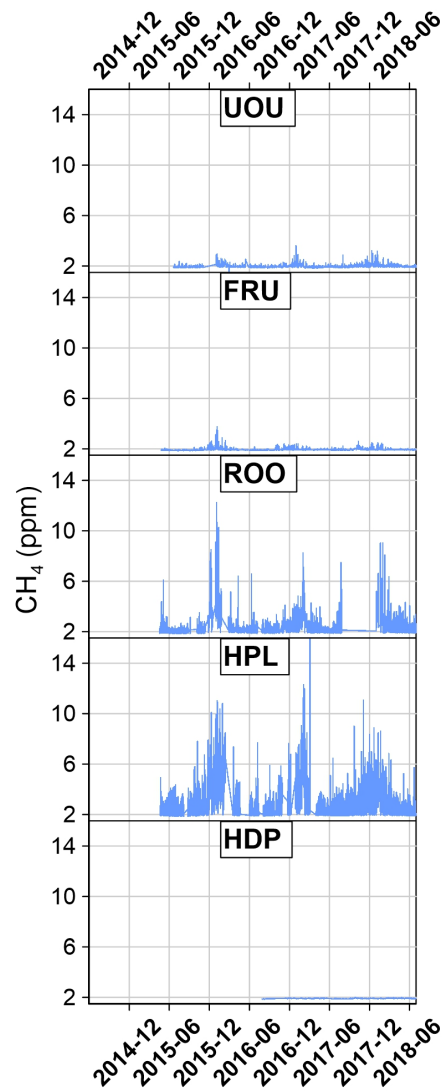


Figure 3: Full record time series of CH<sub>4</sub> measurements from the UUCON and Uintah Basin GHG.

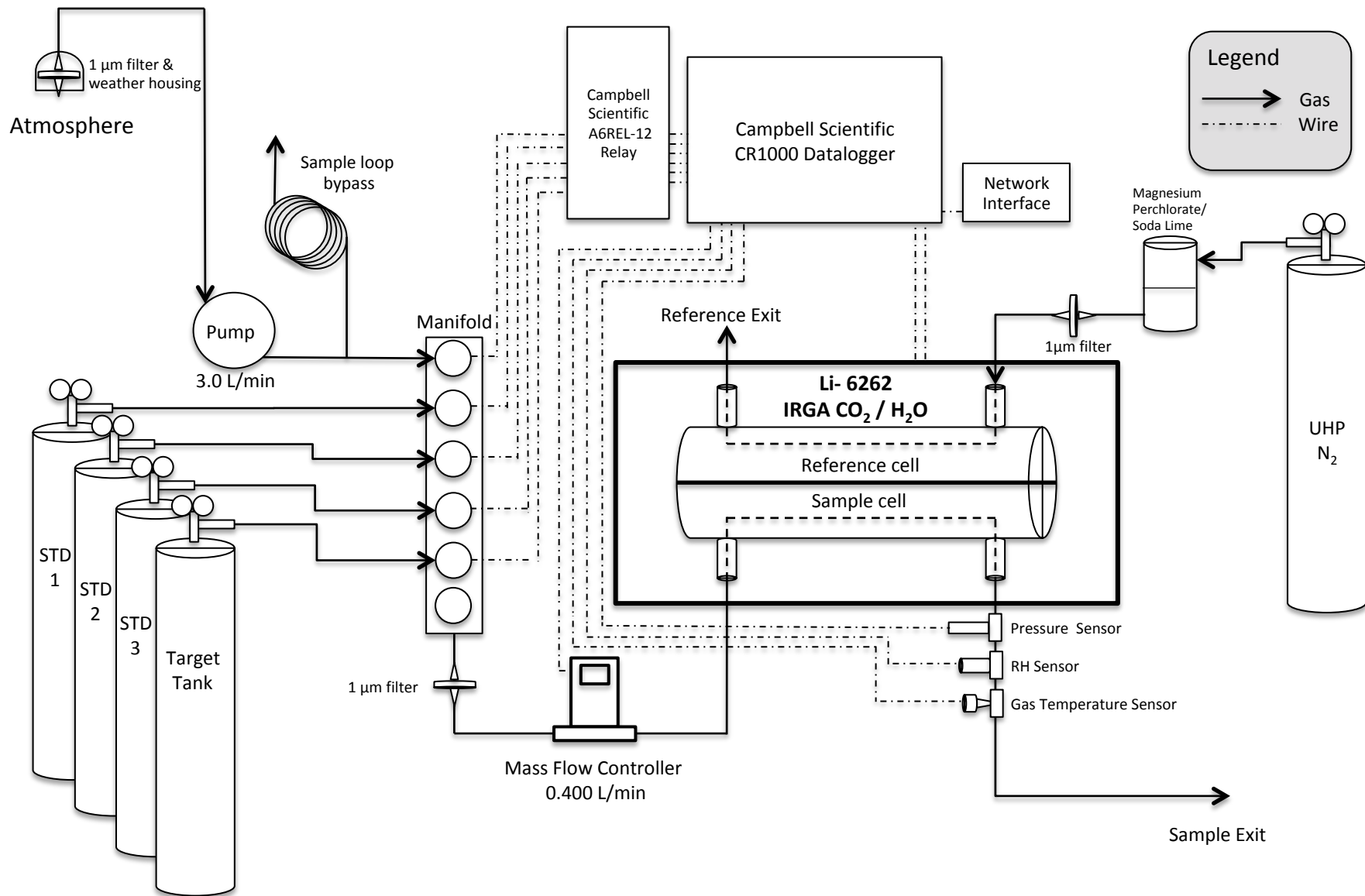


Figure 4: Diagram of UUCON measurement design, not to scale. Sites with this design identified in Fig 1. with blue triangles. STD = Standard Tank.



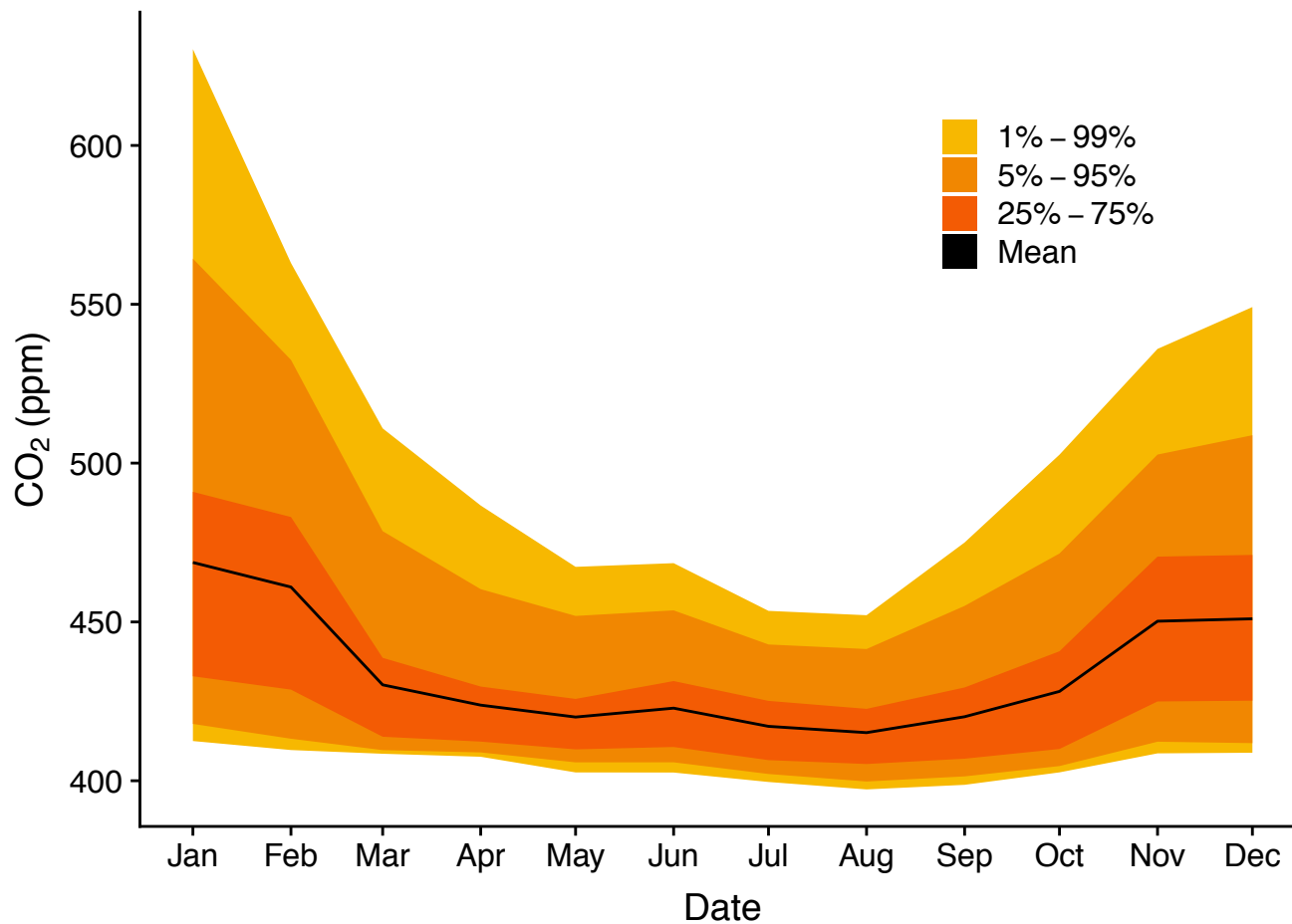


Figure 5: Monthly percentiles of atmospheric observations from SUG over one year, 2017. Note that observations in the 95<sup>th</sup> percentile are greater than 550 ppm CO<sub>2</sub>, well beyond the current WMO calibration scale.

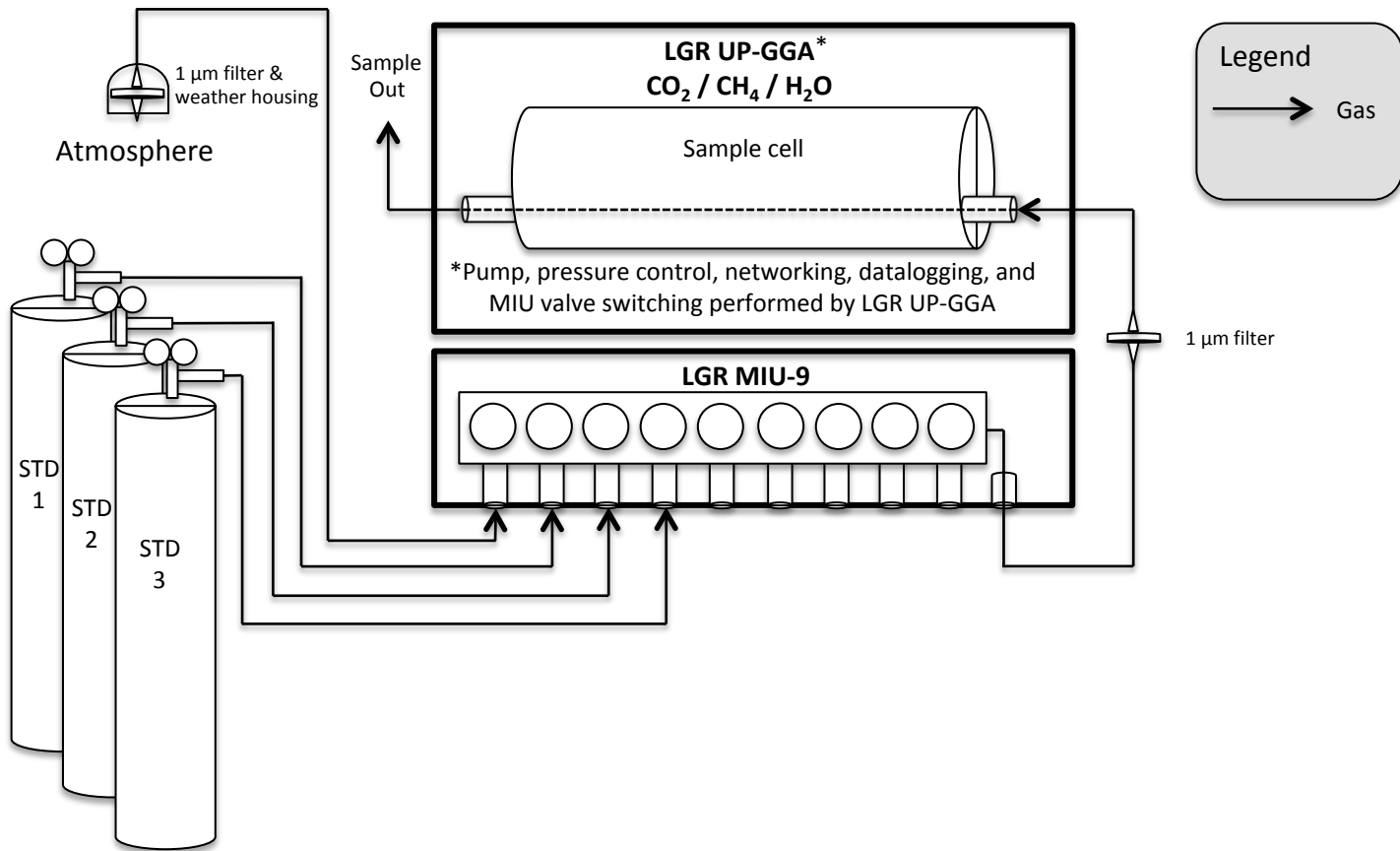


Figure 6: Diagram of Uinta Basin Greenhouse Gas Network measurement design. Sites with this design identified in Fig 1. with red triangles.

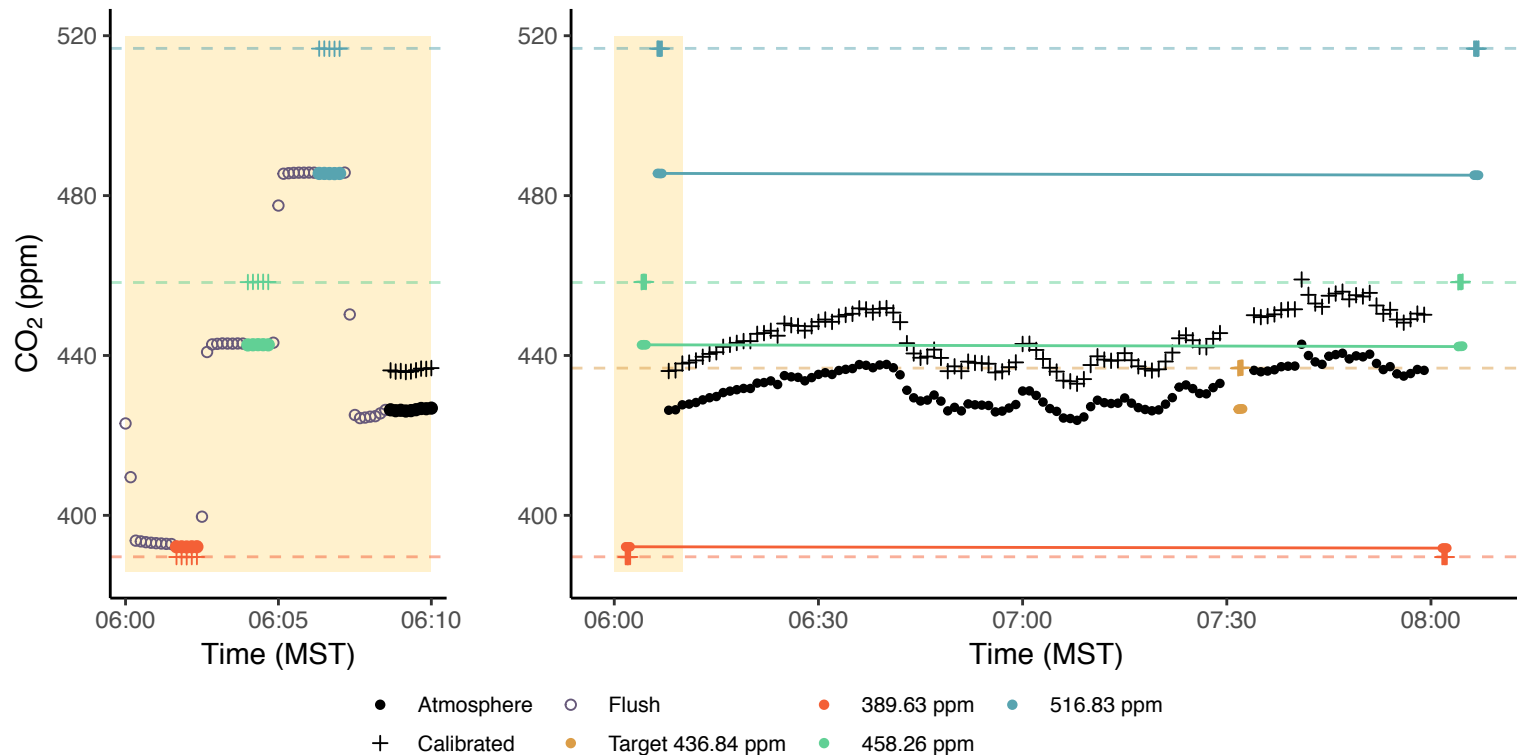


Figure 7: Left panel shows the sequence and timing of a standard calibration period in both the UUCON and Uinta Basin network. Gray open circles indicate the 90 second flushing period observed between each change in gas. Right panel shows a full two hour sample period with calibrations for the UUCON network with linear interpolations; flush periods have been removed. Orange, green, and blue closed circles indicate calibration standard gas and their known CO<sub>2</sub> concentration. Yellow closed circle represents the target tank and its known concentration. Black closed circles indicate pre-calibration atmospheric observations which have been down sampled to one minute averages to reduce over plotting. Plus (+) signs in all colors indicate the calibrated measurements for the corresponding measurement.

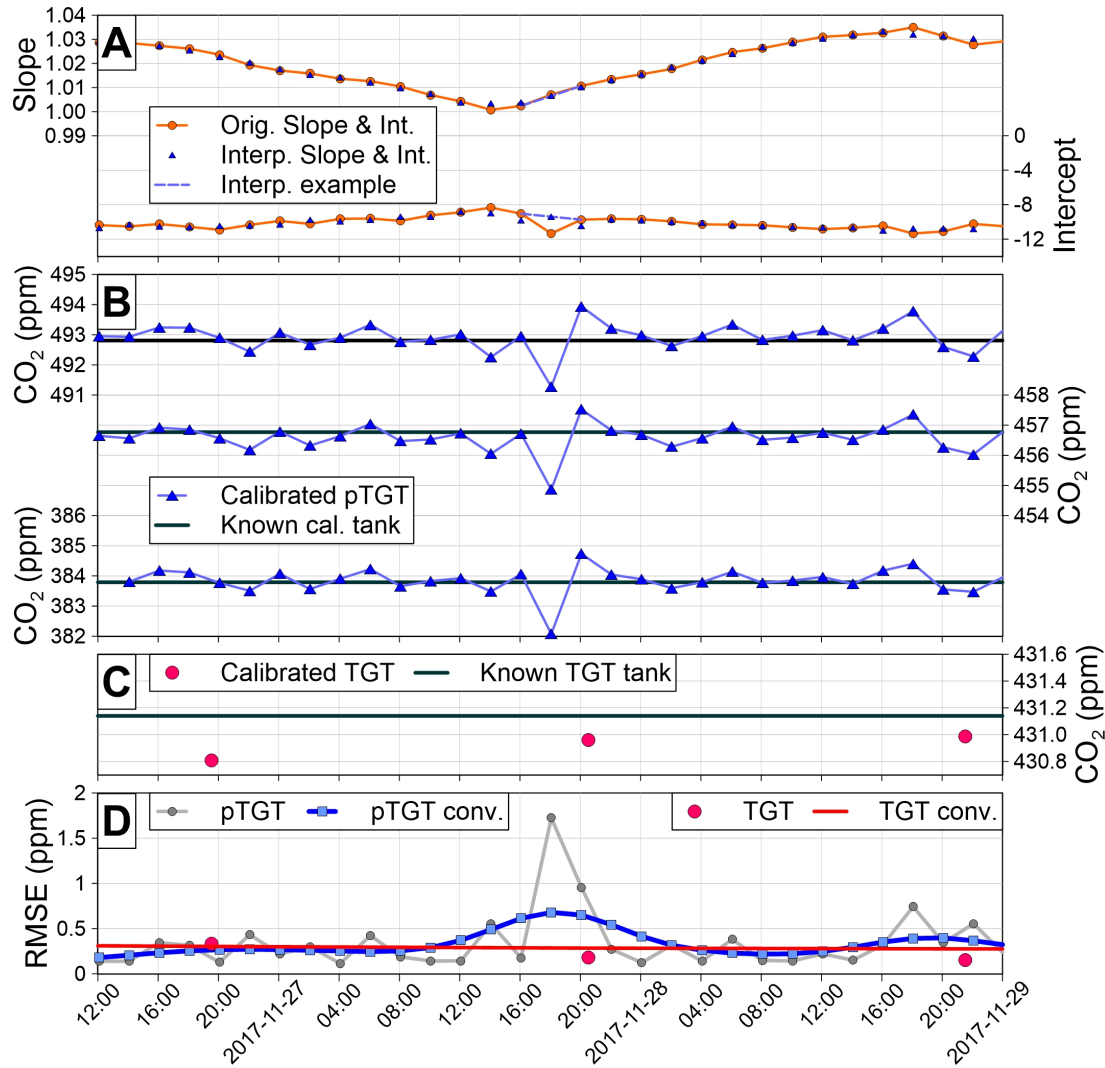


Figure 8: Detailed view of the uncertainty analysis at the IMC site. An example of the interpolation procedure is illustrated for the calibration at 18:00 UTC on November 27, 2017 (see the description in the text). The “pTGT conv.” and “TGT conv.” curves in panel D are the  $U_{\text{pTGT}}$  and  $U_{\text{TGT}}$  uncertainty metrics, respectively.

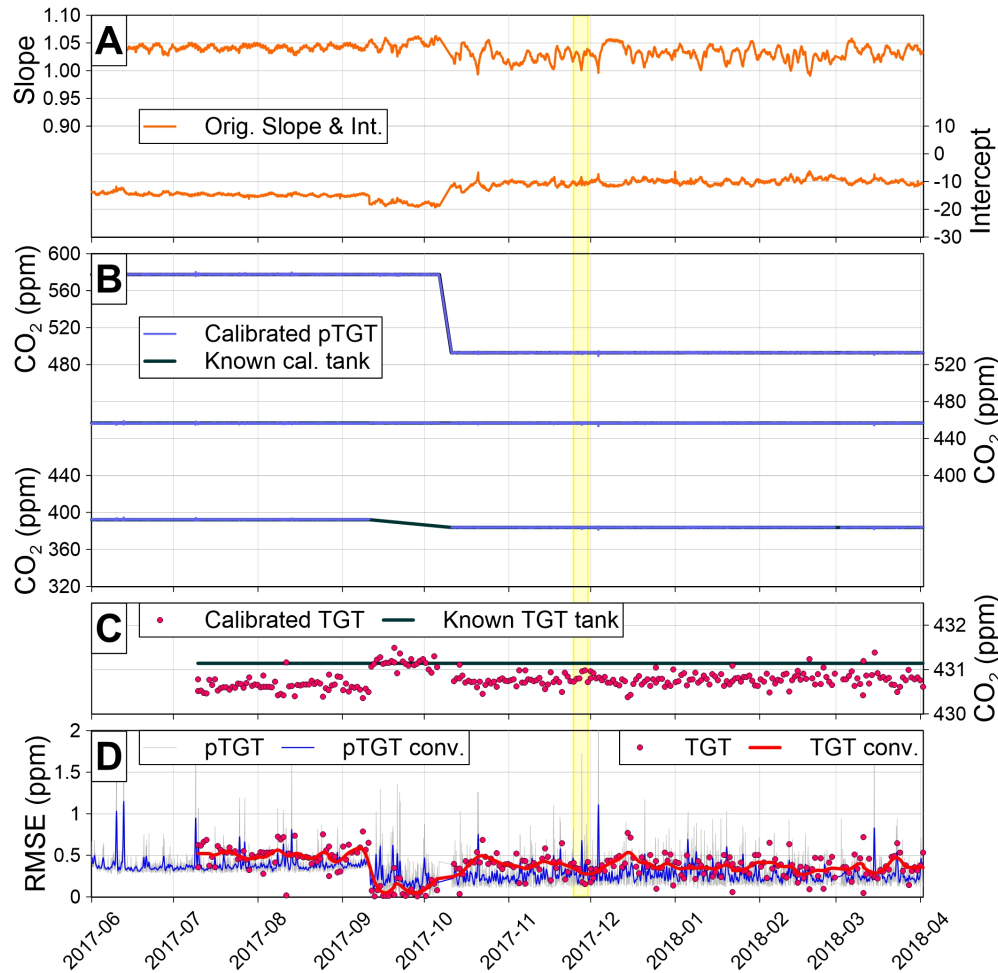


Figure 9: Uncertainty analysis at the IMC site for the time period when a target tank was deployed at the site. The “pTGT conv.” and “TGT conv.” curves in panel D are the  $U_{\text{pTGT}}$  and  $U_{\text{TGT}}$  uncertainty metrics, respectively. The yellow shaded region in Figure 9 is the time period shown in Figure 8. See description in text (section 4) for greater details.

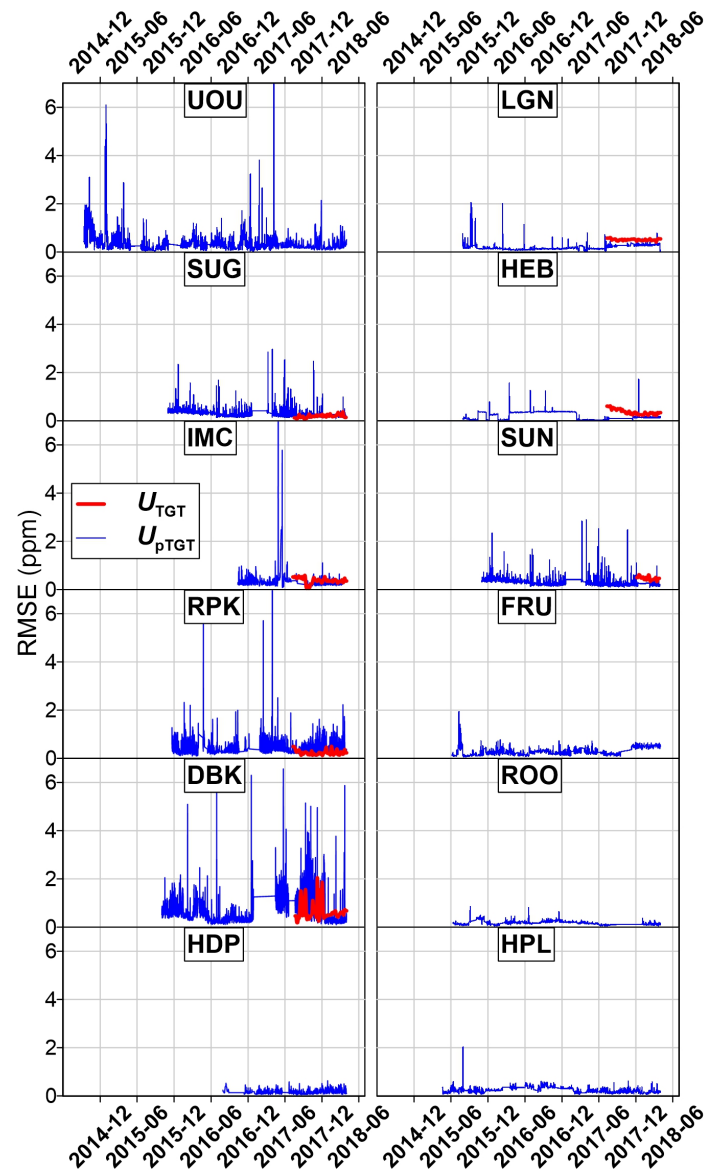


Figure 10: Uncertainty analysis for all of the UUCON sites. The  $U_{pTGT}$  and  $U_{TGT}$  uncertainty metrics are the same as the “pTGT conv.” and “TGT conv” curves in Fig. 8d and 9d, respectively.

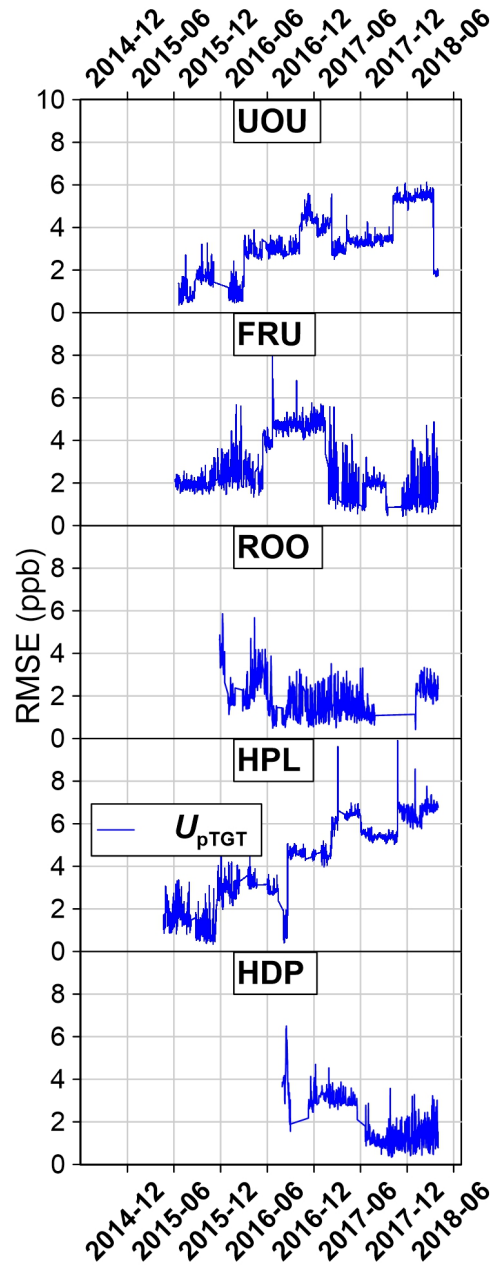


Figure 11: CH<sub>4</sub> Uncertainty analysis. All values reported are the  $U_{pTGT}$  uncertainty metrics as shown in Fig. 9d.